

Imperial College London

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Structural Metamaterials
for frequency control and
vibration mitigation during
launch



Structural Metamaterials Group

- Co-led by Matthew Santer and Rob Hewson in the Department of Aeronautics at Imperial College London
- <https://www.imperial.ac.uk/structural-metamaterials/>
- Design optimization that works in the real world. Generate **manufacturable**, multiscale structures for a range of objectives such as, **stiffness, weight, controlled displacement, failure, uncertainty, frequency** and **vibration modes, thermostructural response, [insert pde here]...**
- Take a look at our poster and models



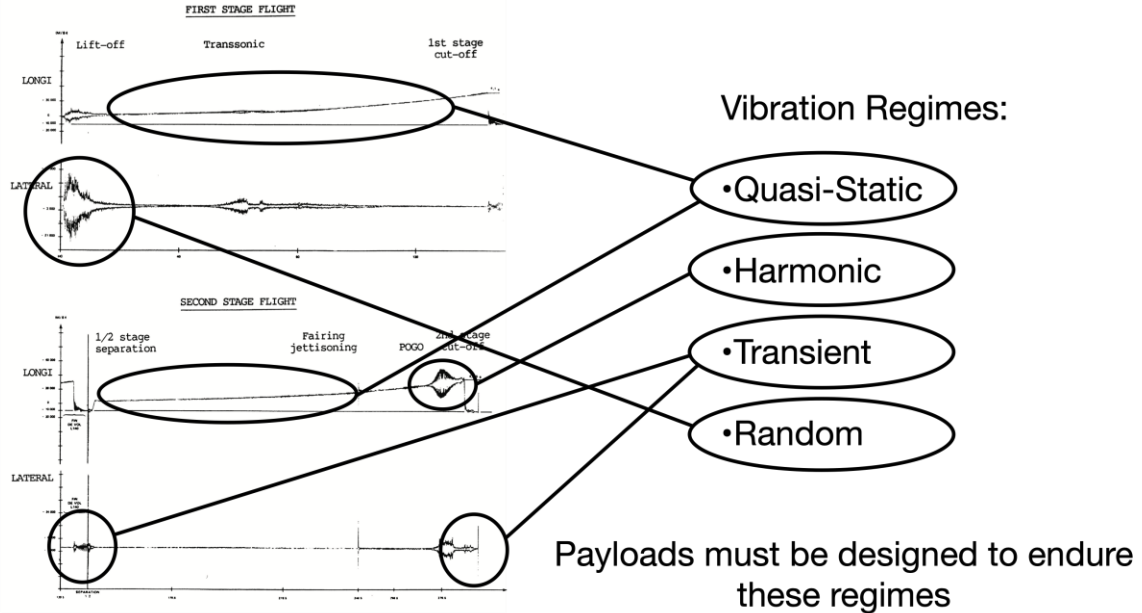
Dynamic Launch Loads

Launch is usually the most challenging environment a spacecraft must endure



© SpaceX Falcon Heavy launch

Ariane 1 first flight data



Launch Qualification

- Launcher specific sinusoidal, random and shock dynamic loading
- Industry standard qualification process
 - Linear finite element analysis in the frequency domain
 - Experimental validation on a shaker
- If the launcher changes so does the launch environment
- Often necessitates a costly and time-consuming redesign
- Use of structural metamaterials avoids this need
 - We can tailor resonant response without changing bulk structural properties

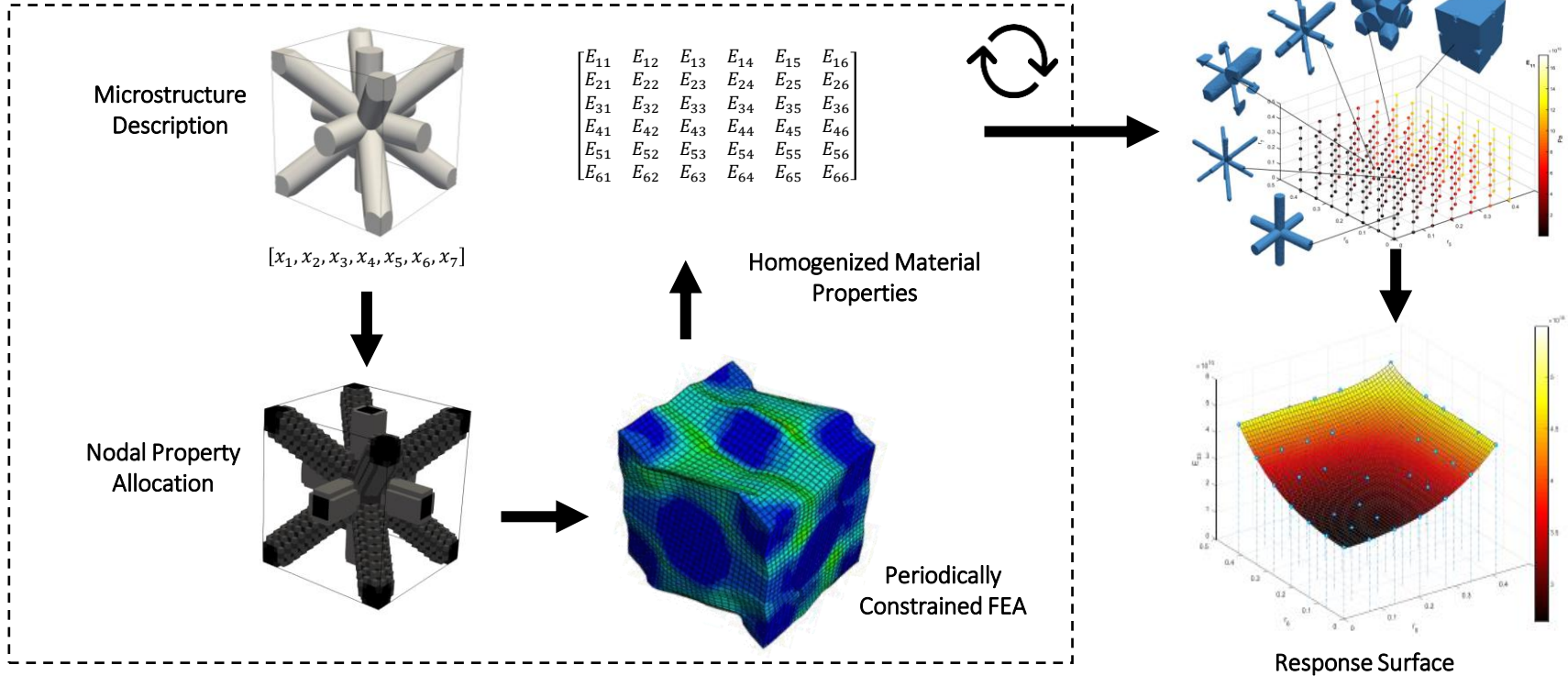


My shaker!

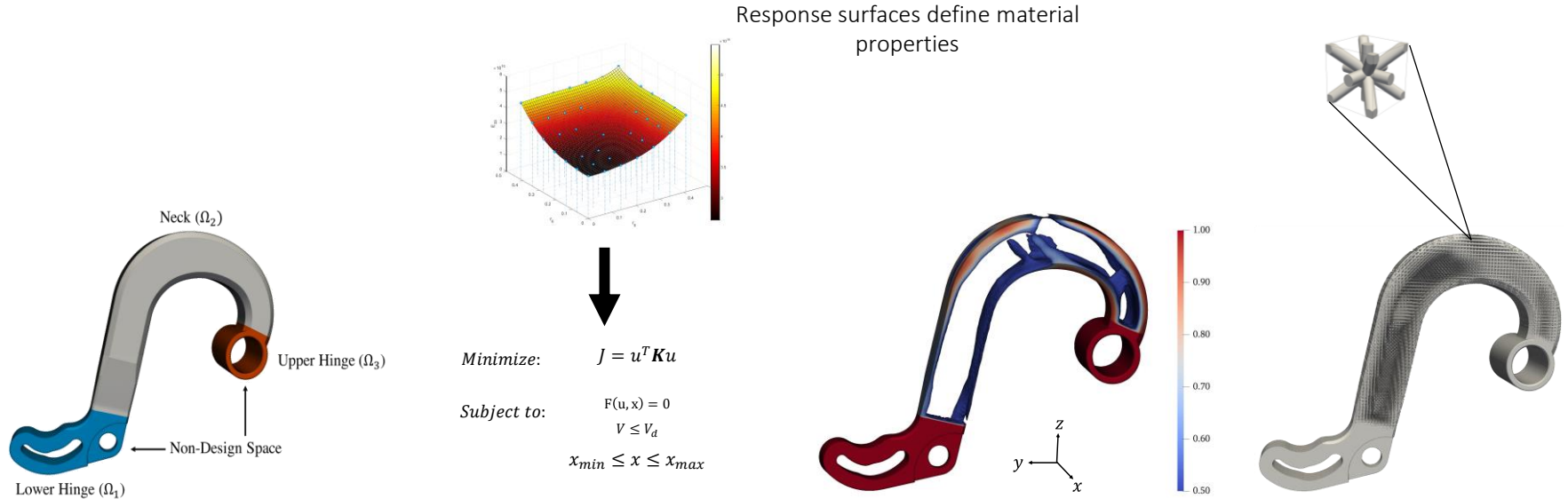


© ESA BepiColumbo vibe test

Microscale Material Properties



Macroscale Optimization



Problem Definition



Optimization loop



Optimization Output



Lattice Reconstruction



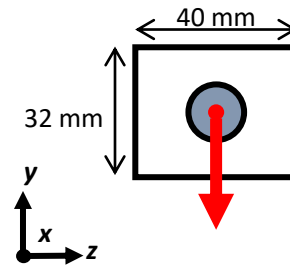
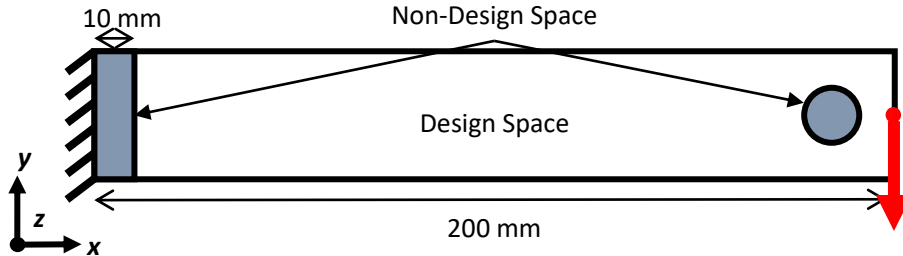
Frequency Tailoring

Frequency Optimization

- $[K - \lambda_i M]\phi_i = 0$ → Resonance eigenvalue equation
- $\omega_i = \frac{\sqrt{\lambda_i}}{2\pi}$ → Eigenvalue to resonant frequency
- $\phi_i^T M \phi_i = 1$ → Mass normalised mode shapes
- $\omega_{lb} \leq \omega_n \leq \omega_{ub}$ or *Max*: ω_n → Frequency constraint or objective

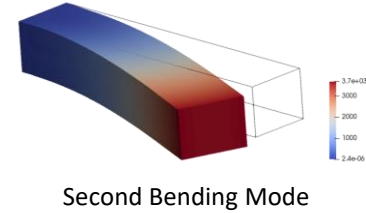
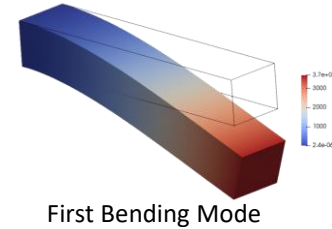
Mode Shape Optimization

- $MAC_i \geq 0.9$ → MAC constraint
- $MAC = \frac{(\varphi^T \phi)^2}{(\varphi^T \varphi)(\phi^T \phi)}$
 - φ is the desired mode shape
 - ϕ is the current mode shape



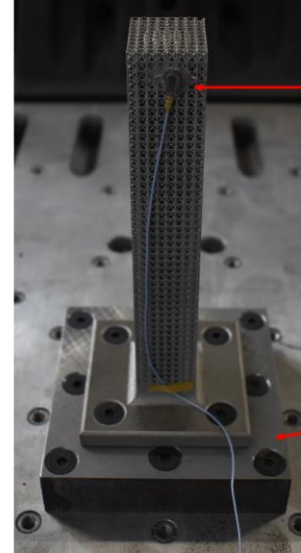
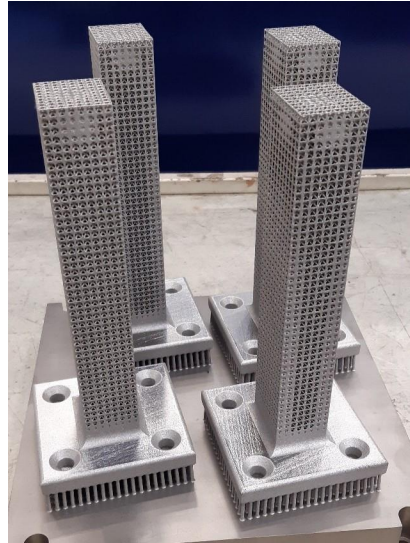
Metamaterial Results

1. Uniform Lattice
2. (Static) Compliance Optimized – No frequency constraints
3. Compliance Optimized – Increase 1st bending mode $\omega_1 \geq 800$
4. Compliance Optimized – Swap the order of frequencies $\omega_2 \leq 650$



| Specimen | Compliance | Volume Fraction, V_D | ω_1 | ω_2 |
|----------|------------|------------------------|------------|------------|
| 1 | 17.74 | 0.4 | 345 | 426 |
| 2 | 5.10 | 0.4 | 757 | 792 |
| 3 | 5.29 | 0.4 | 800 | 878 |
| 4 | 5.17 | 0.4 | 708 | 650 |

Experimental Verification



- Brüel & Kjær 440 mm shaker
- LDS hydrostatic-bearing slip table
- 0.5 g Sinusoidal sweep 10-1000 Hz



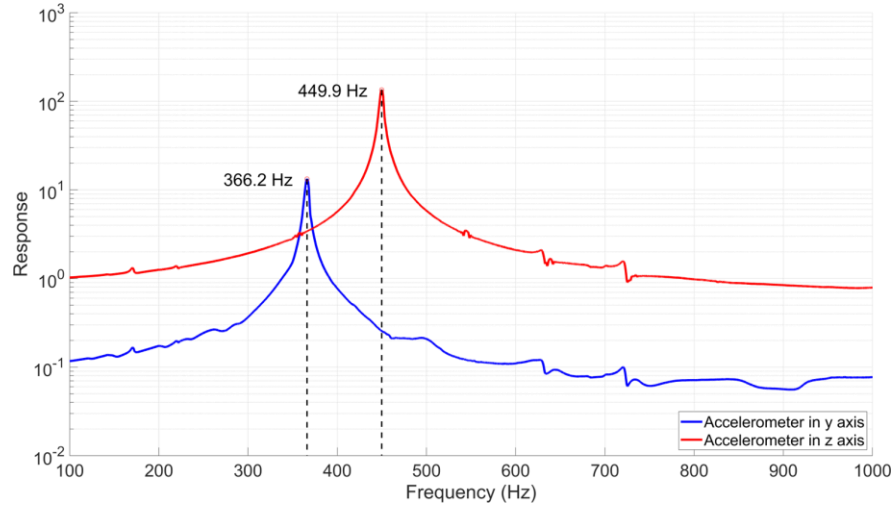
AIRBUS

- EOS M290 Machine
- Titanium Alloy Ti64

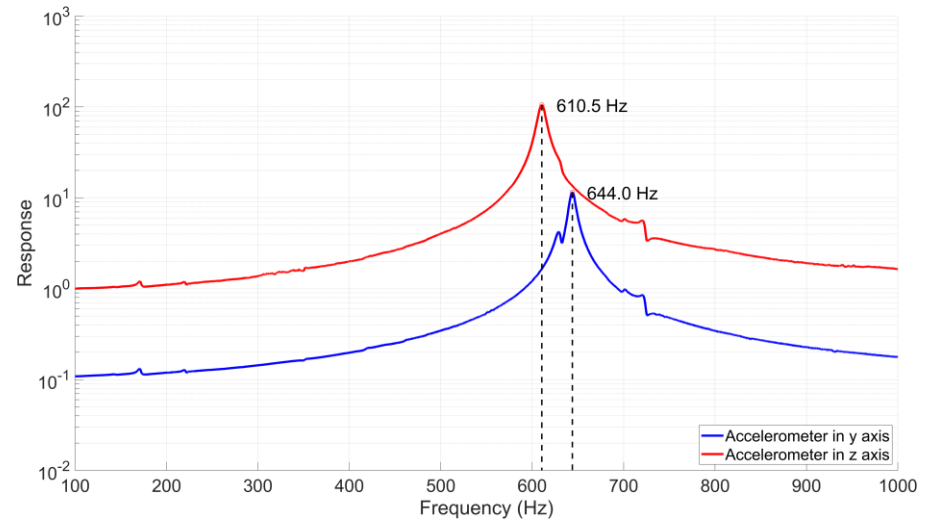
- Heat Treatment
 - 720°C
 - 2 hours
- Ultrasound Bath

Validation Example

Case 1



Case 4



Same mass; same static compliance

Conclusion

- Metamaterials enable frequency tailoring
 - Avoid undesired resonance
 - Enforce band gaps
 - Define mode shapes
- Performance has been validated
- Enables rapid optimal redesign of components whilst maintaining bulk structural properties
- The biggest roadblock is the manufacturing and qualification not the science



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